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(54) Sensor for oxygen-combustibles gas mixtures.

(57) A sensor for detecting the amount of O₂ and combustible gas in a gaseous mixture uses two electrochemical cells (20,40) operating in sequence, to detect oxygen and gaseous combustible contents respectively; the first electrochemical cell (20) is a molten carbonate electrochemical cell operating at a temperature between 400 and 700°C and is used to remove O₂ in combination with CO₂ from the oxygen/combustibles gas mixture to provide a low temperature measurement of the oxygen content of the gas mixture. The second electrochemical cell (40) is an oxygen ion conductive using catalyzing electrodes (44, 46) and an external source of O₂, e.g. air, to cause combustion of the combustible components of the mixture.

The cells (20, 40) each have electrodes (24,26;44,46) applied across cell-walls to apply a potential to cause oxygen transport across the cell walls. The current flowing through across the cell-walls in a measure of either the oxygen content or the oxygen required to oxidize the combustible gaseous contents.

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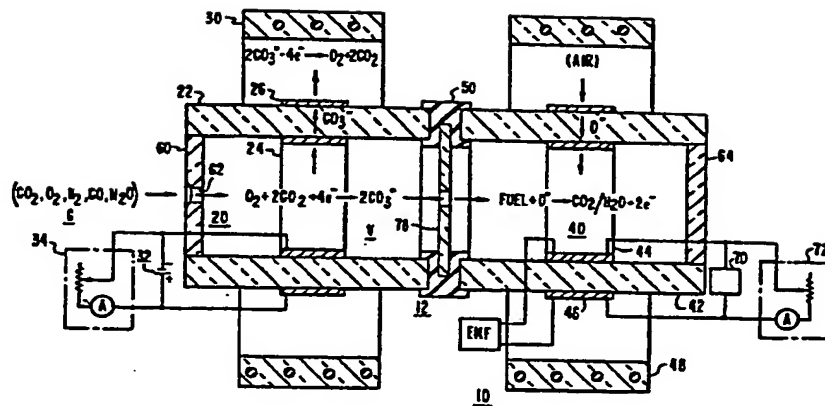


FIG. 1

SENSOR FOR OXYGEN-COMBUSTIBLES GAS MIXTURES

This invention relates generally to gas sensors for measurement of gas compositions in gaseous mixture; more particularly, it relates to a sensor for the quantitative measurement of oxygen in the presence of combustibles, such as hydrogen or carbon monoxide.

Traditional gas analysis methods, such as gas chromatography, can be used for such a purpose, but gas chromatography methods require gas sampling and do not provide the in-situ type of analysis that allows fast control of firing conditions to prevent possible hazard. Thus, it is preferred to use an in-situ probe-type sensor for monitoring these potentially hazardous or explosive conditions.

Conventional electrochemical-potential measurements of commercially available probe-type solid electrolyte sensors are undesirable for this gas measuring application in that such devices operate at temperatures, i.e. 800-1200°C, at which undesirable reactions occur between the oxygen and fuel constituents of a gas mixture, thereby rendering any measurements inaccurate.

There is disclosed herein with reference to the accompanying drawings an electrochemical cell device which obviates certain disadvantages of prior art gas sensors; the cell device disclosed herein separates oxygen and combustibles at a relatively low temperature and allows the measurement of the separated components without encountering undesirable reactions.

The successful operation of the device requires the presence of carbon dioxide or carbon dioxide and water vapor in the gas mixture. The device consists of a molten carbonate electrochemical cell that operates at a temperature of approximately 450°C to 700°C to separate oxygen from the combustibles constituents of the gas mixture and produce a cell current indicative of the oxygen content of the gas mixture. The gross combustibles content of the gas mixture is then measured.

The invention in its broad form consists in an oxygen sensor apparatus for measuring the oxygen content of a gas mixture comprising oxygen and combustible gases wherein said gas mixture includes carbon dioxide, or the combination of carbon dioxide and water vapor besides oxygen, the apparatus comprising:

a molten carbonate electrochemical cell defining a plenum and disposed in use to admit a sample of the mixture of oxygen and combustible gas to be monitored, said plenum comprised of a molten-carbonate-electrolyte wall consisting of a eutectic carbonate mixture impregnated in a porous support and first and second electrodes disposed on and contacting opposite surfaces of said molten-carbonate-electrolyte wall;

means for supplying an oxygen/combustibles gas mixture containing carbon dioxide, or a combination of carbon dioxide and water vapor, besides oxygen into said plenum for contact with the first inside surface of said molten carbonate electrolyte wall;

means for transporting carbon dioxide and a corresponding amount of oxygen for reaction from said gas mixture through said wall to the outside of said plenum to deplete the oxygen present in said gas mixture, said transport of carbon dioxide and oxygen producing an electrochemical cell current; and

means for measuring said cell current as an indication of the oxygen content of said gas mixture.

The invention will become more readily apparent from the following exemplary description when read in conjunction with the accompanying drawings wherein:

Figure 1 is a sectional pictorial illustration of an embodiment of the invention; and

Figure 2 is a sectional pictorial illustration of an alternative embodiment of the invention.

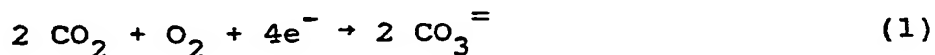
Referring to Fig. 1 there is illustrated in section a gas-constituent-separating and measuring device 10. The typical embodiment of the device 10 as shown in Figure 1 consists of a tubular enclosure 12 consisting of a tubular molten carbonate electrochemical cell 20 and a tubular oxygen ion conductive solid electrolyte electrochemical cell 40 secured in an end-to-end relationship by a sealing member 50. A gas diffusion limiting adapter, or orifice plate 60 is positioned at one end of the tubular enclosure 12 to accommodate the diffusion of the constituents, i.e., CO_2 , O_2 , H_2 , CO , etc. from an oxygen/combustibles gas environment G through the aperture 62 into the internal volume V of the tubular enclosure 12. The opposite end of the tubular enclosure 12 is closed by the end plate 64. The molten-carbonate electrochemical cell 10 consists of a molten carbonate electrolyte 22 and electrodes 24 and 26 disposed on opposite surfaces thereof. The oxygen ion conductive solid electrolyte electrochemical cell 40 consists of an oxygen ion conductive solid electrolyte member 42 and electrodes 44 and 46 disposed on opposite surfaces thereof. The seal 50 is of a material suitable for withstanding the mechanical vibration and temperature of operation of the device 10.

The molten carbonate electrochemical cell 20 is operated at a temperature in a range between approximately 400°C and 700°C which is maintained by the furnace 30 within which the cell 20 is positioned. The oxygen ion conductivity operation of the cell 40, necessitates an operating temperature between 700°C and 1200°C , which is established and maintained by the furnace 48 within which

the cell 40 is positioned. The cell 40 typically consists of a solid electrolyte material consisting of stabilized zirconia, and electrodes 44 and 46 of platinum. The composition and operation of the oxygen ion conductive cell 40 is well known in the art, and is typically described and illustrated in United States reissue patent 28,792 which is assigned to the assignee of the present invention and incorporated herein by reference.

The molten carbonate electrolyte 22 of the cell 20 consists of a eutectic carbonate mixture impregnated in a porous mechanical support of a suitable non-reactive ceramic, such as lithium aluminate. Suitable eutectic carbonate mixtures include mixtures of Li_2CO_3 , K_2CO_3 , Na_2CO_3 and Cs_2CO_3 which melt at temperatures below 500°C and exhibit high $\text{CO}_3^{=}$ conductivity. The electrodes 24 and 26 are non-catalytic electrodes constructed of noble metals or conducting oxides such as lithiated nickel oxide or silver, copper oxide or magnetite.

The constituents of the monitored gas environment G, which is assumed to include CO_2 , or a combination of CO_2 and water vapor, in excess of O_2 , and constituents such as CO and H_2 , as would typically be present in a combustion process, enter initially that portion of the volume V within the molten carbonate electrochemical cell 20. Under the influence of a voltage of up to 1.5 volts of the polarity indicated applied to the electrodes 24 and 26 of the molten carbonate cell 20 by the voltage source 32, the total oxygen content in the gas mixture present within the tubular cell 20 is transported through the molten carbonate electrolyte 22 by an equivalent amount of CO_2 in accordance with the following reaction at the cathode electrode 24:



and oxygen will be released at the anode electrode 26 by the reaction:



A current-measuring circuit 34 connected to the electrodes 24 and 26 measures the current developed by the molten carbonate cell 20 in response to the transfer of oxygen by the carbon dioxide via carbonate ions as an indication of the oxygen concentration in the monitored gas environment G.

10 In the event water vapor is present in the gas mixture and hydroxides accumulate in the molten carbonate electrolyte 22, hydroxide carbonate mixtures can develop as the water vapor can transfer oxygen through the electrolyte via hydroxyl ions.

15 The molten carbonate electrolyte 22 effectively supports the transfer of O_2 with CO_2 from the internal volume in response to the applied potential from the voltage source 32 at operating temperatures of between approximately 400 and 700°C as controlled by the furnace
20 30. This low temperature of operation of the molten carbonate cell 20 avoids the possibility of initiating a chemical reaction between the fuel and oxygen constituents of the monitored gas environment entering the device 10 prior to the removal or separation of the oxygen constituent
25 from the gas mixture entering the device 10 through the aperture 62. The combustibles constituent(s), i.e. H_2 , is then transported to the portion of the internal volume V of the device 10 enclosed by the oxygen ion conductive solid electrolyte cell 40. A voltage source 70
30 is connected across the electrodes 44 and 46 to maintain a flow of oxygen from an external oxygen source, such as air, through the solid electrolyte member 42 into the volume enclosed by the cell 40 to combustively react with the fuel constituent in the presence of a catalytic elec-
35 trode 44, which is typically platinum, at the operating

temperature of the cell 40 which is typically in excess of 800°C. The cell current generated by the transport of the oxygen ions, is measured by the current measuring circuit 72 as an indication of the gross combustibles content of the monitored gas environment G.

While the voltage source 70 provides a means for maintaining a steady applied potential, the self-generated EMF of the cell 40 resulting from the oxygen differential partial pressure across the electrolyte 42 can be employed to effect the desired transfer of oxygen to combustibly react with the fuel constituents of the gas mixture at the catalytic electrode 44.

It is apparent that the device 10 of Figure 1 can consist solely of the molten carbonate cell 20 if only an oxygen measurement is required.

As an alternative, an EMF measuring circuit can be connected across the electrodes 44 and 46 of the cell 40, as described in the above-identified U.S. reissue patent, to provide an oxygen measurement in accordance with the well-known Nernst equation, assuming a known or steady oxygen reference, such as air, at the electrode 46. This well-known technique for providing an oxygen measurement can indirectly provide a measure of the concentration of combustibles inasmuch as the low temperature oxygen concentration measured by the molten carbonate cell 20 will differ from that measured by the high temperature operation solid electrolyte cell 40 by the amount of oxygen that is consumed by the presence of combustibles at the elevated operating temperature of the cell 40.

An optional gas diffusion aperture element, or orifice plate, 78 can be employed between the internal volumes of the device 10 defined by the cells 20 and 40 to provide a range selection control by limiting the amount of gas entering the cell 40.

Referring to Figure 2, there is illustrated in a sectioned schematic form an alternative embodiment which eliminates the need for the high temperature oxygen ion

conductive electrochemical cell 40 of Figure 1 and employs two molten carbonate electrochemical cells 80 and 90 which share a single furnace 99 which maintains the two cells at a common operating temperature of between 400°C and 700°C.

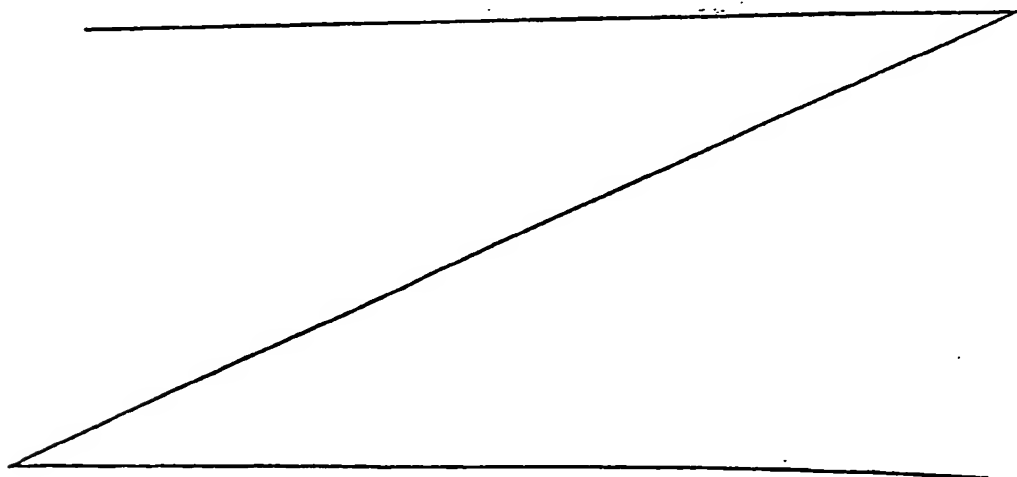
5 The configuration of Figure 2 eliminates the separate heating levels of the embodiment of Figure 1 and further eliminates the need for the sealing means 50. In the implementation of the device 10 of Figure 2 the oxygen and combustibles content of the gas mixture are measured by
10 the dual molten carbonate cell combination of cells 80 and 90 which may consist of separate electrolytes or share a single common molten carbonate electrolyte 82. The gas mixture passing through the aperture 62 of the gas diffusion limiting adapter 60 first enters the internal volume
15 defined by the tubular molten carbonate electrochemical cell 80. As described above with reference to the operation of the molten carbonate cell 20 of Figure 1, the cell 80 responds to the applied potential from source 83 to the non-catalytic electrodes 82 and 84 by transporting CO_2 and
20 a corresponding amount of O_2 from the internal volume through the electrolyte 88 in accordance with equation (1) above. The current developed by the cell 80, and measured by the current measuring circuit 85 is a measurement of the oxygen concentration of the gas mixture diffusing
25 through the aperture 62. The non-catalytic electrodes 82 and 84 of the cell 80 may be constructed from copper, nickel, cobalt, silver, gold and electronically conducting metal oxides except the oxides of the platinum group elements.

30 The combustibles constituent(s) remaining following the removal of the oxygen by the operation of the cell 80 enter the internal volume defined by the molten carbonate cell 90. The electrodes 92 and 94 are catalytic electrodes, i.e., typically platinum. The oxygen reference environment of cell 40 of Figure 1 is replaced by an
35 external gas mixture of O_2 and CO_2 surrounding the cell 90

and in contact with the electrode 94. An electrical potential as shown is applied across electrodes 94 and 92 by the voltage source 95 to produce a transport of CO_2 and an equivalent amount of O_2 through the molten carbonate electrolyte 88 to the internal volume of the device 10 defined by the cell 90. The introduction of oxygen to this internal volume to contact the combustible content present at the surface of the catalytic electrode 92 results in the electrochemical combustion of the combustible constituents or fuel constituent(s) within the volume of the cell 90. The current produced by the cell 90, as measured by the current measurement circuit 97 is an indication of the gross combustibles content of the gas mixture entering the diffusion orifice 62.

As discussed above with reference to the voltage source 70 of Figure 1, the voltage source 95 can be eliminated and the self-generated EMF of the cell 90 employed to transfer O_2 to combustibly react with the fuel constituents of the catalytic electrode 92.

As discussed above with reference to the embodiment of Figure 1, an optional gas diffusion limiting aperture adapter 100 can be inserted to partition the internal volumes defined by the cells 80 and 90, respectively, to provide capability of range selection by limiting the fuel constituent gas mixture entering the volume defined by the cell 90.



What we claim is:

1. An oxygen sensor apparatus for measuring the oxygen content of a gas mixture comprising oxygen and combustible gases wherein said gas mixture includes carbon dioxide, or the combination of carbon dioxide and water vapor besides oxygen, the apparatus comprising:
 - a molten carbonate electrochemical cell defining a plenum and disposed in use to admit a sample of the mixture of oxygen and combustible gas to be monitored, said plenum comprised of a molten-carbonate-electrolyte wall consisting of a eutectic carbonate mixture impregnated in a porous support and first and second electrodes disposed on and contacting opposite surfaces of said molten-carbonate-electrolyte wall;
 - means for supplying an oxygen/combustibles gas mixture containing carbon dioxide, or a combination of carbon dioxide and water vapor, besides oxygen into said plenum for contact with the first inside surface of said molten carbonate electrolyte wall;
 - means for transporting carbon dioxide and a corresponding amount of oxygen for reaction from said gas mixture through said wall to the outside of said plenum to deplete the oxygen present in said gas mixture, said transport of carbon dioxide and oxygen producing an electrochemical cell current; and
 - means for measuring said cell current as an indication of the oxygen content of said gas mixture.

2. A sensor apparatus as claimed in claim 1 further including means for heating said molten carbonate electrochemical cell to a temperature predetermined range to enhance the conductivity of said molten carbonate cell while limiting said temperature to a level less than that at which a combustible reaction would occur between the oxygen and combustibles constituents of said gas mixture.

3. A sensor apparatus as claimed in claim 1 wherein said eutectic carbonate mixture comprising said molten carbonate electrolyte wall is a mixture selected from the following: Li_2CO_3 , K_2CO_3 , Na_2CO_3 , and Cs_2CO_3 .

4. A sensor apparatus as claimed in claim 1 wherein said porous support is of non-reactive ceramic material consisting of lithium aluminate.

5. The sensor apparatus as claimed in claim 1 wherein said first electrode is a noncatalytic electrode.

6. A sensor apparatus as claimed in claim 2 wherein said means for heating maintains said molten carbonate electro-chemical cell wall at a temperature approximately between 400 and 700°C.

7. A gas sensor apparatus as in claim 1 including a second electrochemical cell means having an electrolyte and third and fourth electrodes disposed on and contacting opposite surfaces thereof, said third electrode being a catalytic electrode, the gas mixture devoid of the oxygen content which was depleted by said molten carbonate electrochemical cell flowing to contact said third electrode of said second electrochemical cell, an external oxygen gas environment being provided to contact said second electrode of said second electrochemical cell,

means for transporting oxygen from said external oxygen gas environment to the third electrode surface of said second electrochemical cell, said third electrode being a catalytic electrode causing a combustible reaction between the oxygen and the combustible constituents of said gas mixture the transporting of said oxygen producing a cell current in said second electrochemical cell means, and

means for measuring the cell current of said second electrochemical cell to give an indication of the content of combustible gases in the oxygen/combustibles gas mixture.

5 8. A gas sensor apparatus as claimed in claim 7 wherein said second electrochemical cell is a molten-carbonate-electrochemical cell, said external oxygen gas environment contacting said fourth electrode including CO_2 , said means for applying a voltage across the elec-
10 trodes of said second electrochemical cell means transporting CO_2 and a corresponding amount of O_2 through said molten carbonate electrochemical cell to said third electrode.

15 9. A sensor apparatus as claimed in claim 8 wherein said eutectic carbonate mixture comprising said molten carbonate electrolyte is a mixture selected from the following: Li_2CO_3 , K_2CO_3 , Na_2CO_3 , and Cs_2CO_3 .

20 10. A sensor apparatus as claimed in claim 7 wherein said porous support is a non-reactive ceramic unit consisting of lithium aluminate.

25 11. A gas sensor apparatus as claimed in claim 7 wherein said second electrochemical cell is an oxygen ion conductive solid electrolyte electrochemical cell, said means for transporting oxygen consisting of a voltage source connected across the electrodes of said second electrochemical cell means to pump oxygen from said oxygen gas environment to said third electrode.

30 12. A gas sensor apparatus as claimed in claim 11 further including means for heating said molten carbonate electrochemical cell to a temperature approximately between 400 to 700°C and heating said oxygen ion conductive solid electrolyte cell to a temperature of approximately 800°C or higher.

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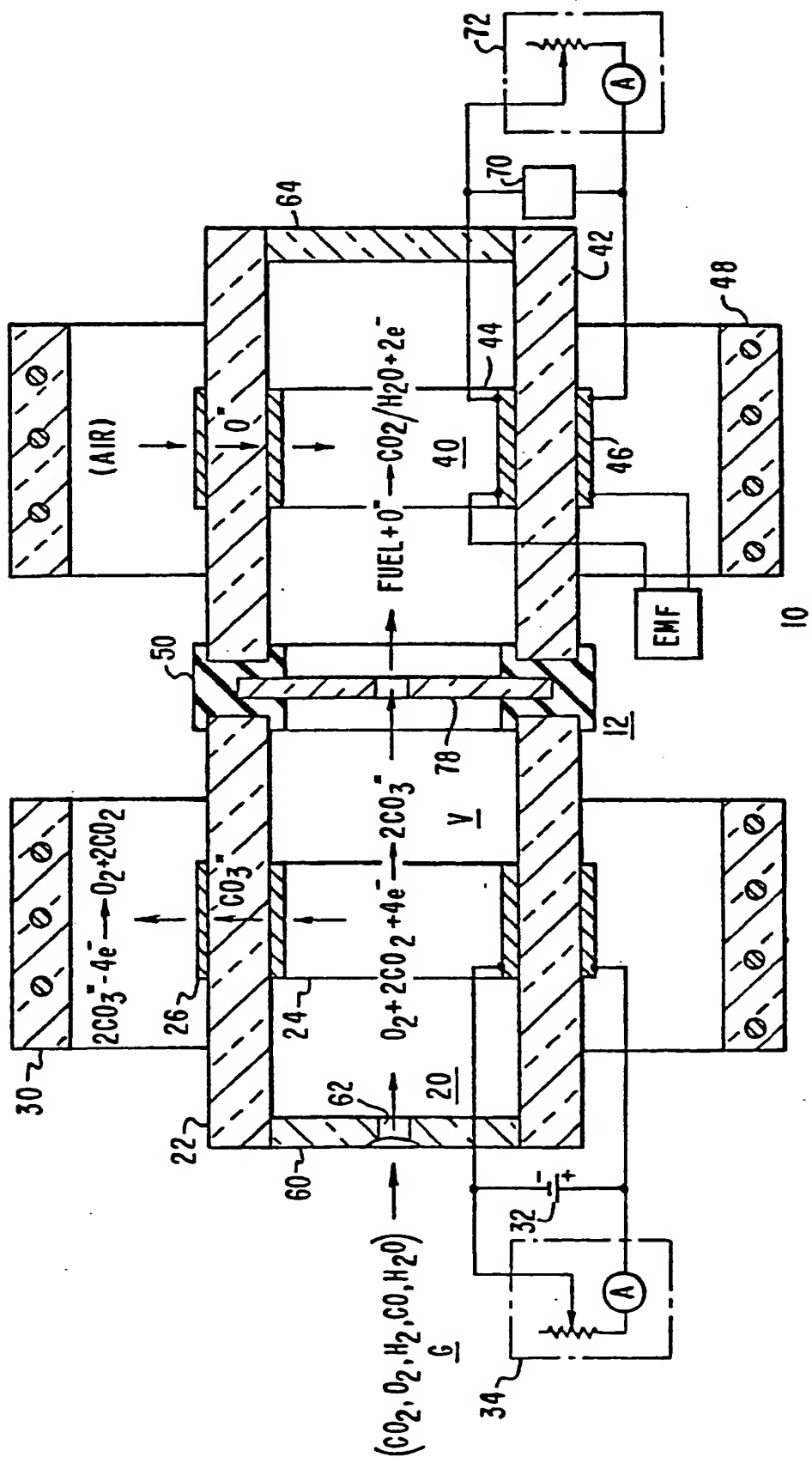


FIG. 1

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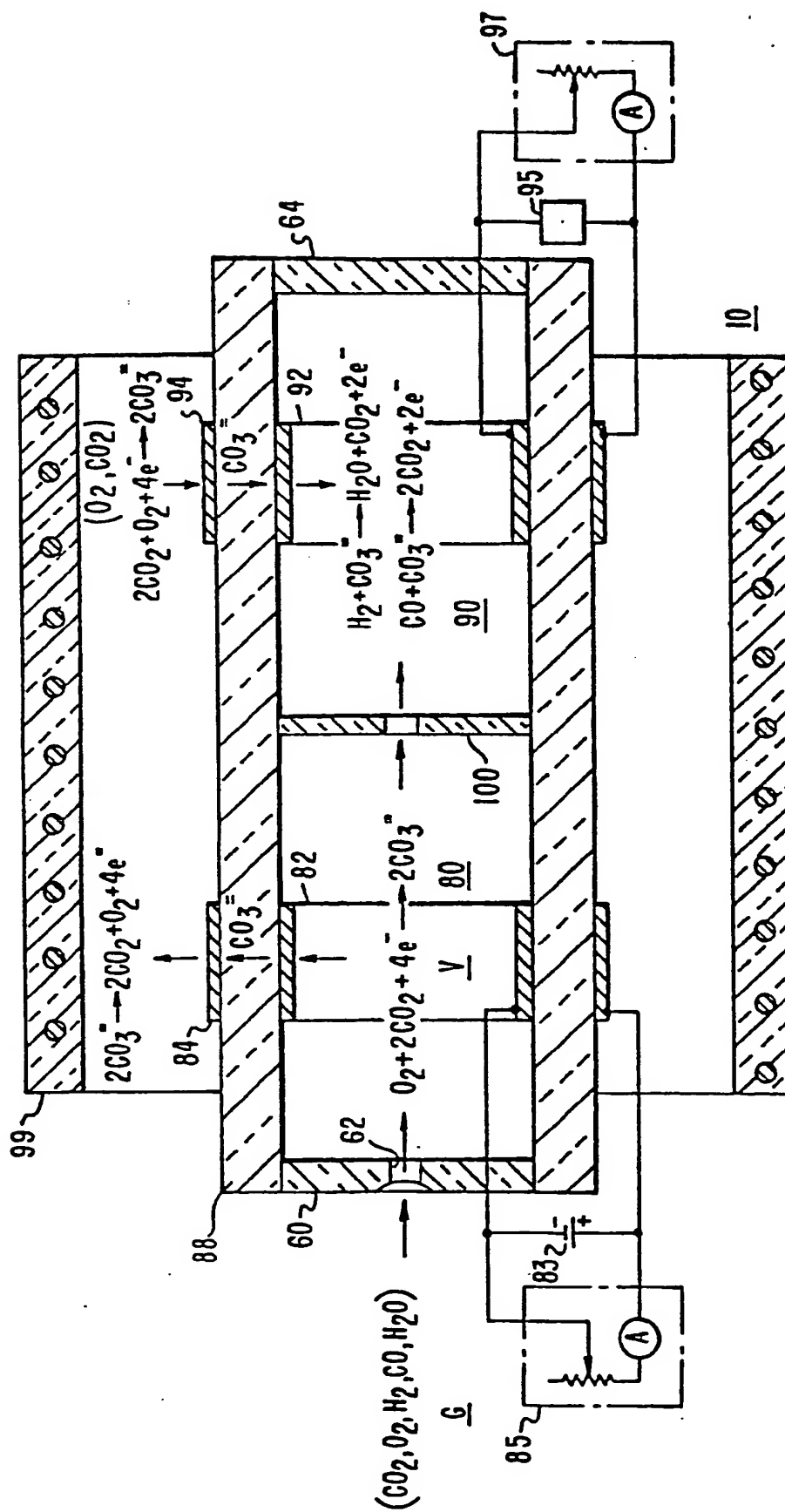


FIG. 2



European Patent
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EUROPEAN SEARCH REPORT

0060944

Application number

EP 81 30 1220.0

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl.)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
	<u>US - A - 3 860 498</u> (W.J. JONES) * claims 5, 6, 7; column 1, lines 33 to 39, 40 to 64; column 3, lines 34 to 68; column 4; fig. 3 *	1,7,11	G 01 N 27/46 G 01 N 33/22 H 01 M 8/14
	<u>US - A - 4 160 067</u> (E.H. CAMARA et al.) * column 3, lines 39 to 56; column 4, lines 37 to 56; column 5, lines 51 to 55 *	1,2,4, 6-8, 10-12	
	<u>US - A - 4 079 171</u> (L.G. MARIANOWSKI et al.) * claims 1, 2, 8; column 1, lines 1 to 63; column 3, lines 13 to 68; column 4, lines 1 to 10 *	4,6,10, 12	TECHNICAL FIELDS SEARCHED (Int. Cl.) G 01 N 1/00 G 01 N 25/00 G 01 N 27/00 G 01 N 33/22 H 01 M 4/00 H 01 M 6/00 H 01 M 8/00 H 01 M 10/00
	<u>US - A - 4 009 321</u> (B.S. BAKER et al.) * column 1, lines 11 to 49; column 2, lines 44 to 60 *	1,2,4, 6-8, 10-12	CATEGORY OF CITED DOCUMENTS X: particularly relevant A: technological background O: non-written disclosure P: intermediate document T: theory or principle underlying the invention E: conflicting application D: document cited in the application L: citation for other reasons
X	The present search report has been drawn up for all claims		&: member of the same patent family, corresponding document
Place of search Berlin		Date of completion of the search 15-12-1981	Examiner DIETRICH

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